

$$v = (1 - x^v) v^L + x^v v^v$$

↳ título vapor

Gas ideal

$$pv = RT$$

Van der Waals

$$\left(p + \frac{a}{v^2}\right)(v - b) = RT$$

$a \propto f. \text{ interm.}$

$$b = N_a \cdot \frac{2\pi}{3} d^3 = 4 N_a V$$

$$a = \frac{3}{8} RT_c \sigma_c$$

$$b = \frac{\sigma_c}{3}$$

$$\left. \begin{array}{l} \\ \end{array} \right\} R = \frac{8}{3} \frac{p_c \sigma_c}{T_c}$$

$$X_r = \frac{X}{X_c}$$

$$\left(p_r + \frac{3}{\sigma_r^2}\right)(3\sigma_r - 1) = 8T_r \quad \text{Ley estados correspondientes}$$

Virial

$$pv = RT \left(1 + \frac{B}{v} + \frac{C}{v^2} + \dots\right) = RT + B'p + C'p^2 + \dots$$

$$\hookrightarrow Z = \frac{pv}{RT}$$

Fugacidad

$$\left(\frac{\partial G}{\partial n}\right)_{T,p} = \mu$$

$$d\mu = -s dT + v dp, \quad dT = 0$$

Gas ideal $\rightarrow \mu = \mu^* + RT \ln p$

No ideal $\rightarrow \mu = \mu^* + RT \ln f$... nueva variable de estado

$$d\mu = RT d \ln f = v dp$$

$$d \ln f = \frac{v}{RT} dp$$

$$\ln f = \ln p + \int_0^p \left(\frac{v}{RT} - \frac{1}{p}\right) dp$$

$$\mu_i = \mu_i^* + RT \ln f_i$$

$$\mu^* = \mu(T, p^* = 1)$$

Sól-Liq

$$f_1^S = f_1^V \quad \text{o} \quad f_2^V = f_2^L$$

$$\ln f_2^S - \ln f_1^S = \frac{1}{RT} \int_{p_1}^{p_2} v^S dp$$

1er orden

$$dQ = Ldn''$$

$$L = h'' - h'$$

$$L = T(s'' - s')$$

$$\mu' = \mu''$$

$$\Rightarrow \frac{dp}{dT} = \frac{s'' - s'}{v'' - v'} = \frac{L}{T(v'' - v')}$$

$$\frac{d \ln p}{dT} = \frac{L}{RT^2} \quad \text{Ecuación de Clapeyron}$$

$$\frac{dL}{dT} = c_p'' - c_p' + \frac{L}{T} \left(1 + \frac{T(\alpha'v' - \alpha''v'')}{v'' - v'} \right) = \left(\frac{ds}{dT} \right)_{SAT} = c_{SAT}$$

$$c_{SAT}^v = c_p^v - T\alpha v \left(\frac{dp}{dT} \right)_{SAT} \quad \left(\frac{ds''}{dT} \right)_{SAT} - \left(\frac{ds'}{dT} \right)_{SAT} = \frac{1}{T} \frac{dL}{dT} - \frac{L}{T^2}$$

$$\text{Vapor: } \frac{dL}{dT} = c_p^v - c_p'$$

$$L \, dm = m c_{SAT}^L \, dT \quad (\text{extr. vapor función hielo})$$

$$\frac{\vec{\nabla} p}{\rho} = - \frac{\vec{\nabla} \psi}{\rho} = - \alpha \vec{\nabla} T$$

TEMA 11

Molaridad $c = \frac{n_2}{V}$ V/dm^3

Molalidad $m = \frac{n_2}{m_1}$

F. m3sica $w_2 = \frac{m_2}{m_1 + m_2} \cdot 100$

$$c = \frac{\rho x_2}{x_2(M_2 - M_1) + M_1}$$

$$m = \frac{(1000) \cdot x_2}{M_1(1 - x_2)}$$

$$F = \sum n_i f_i$$

$$\sum n_i df_i = \left(\frac{\partial F}{\partial T} \right)_{p, n_j} dT + \left(\frac{\partial F}{\partial p} \right)_{T, n_j} dp$$

$$v_2 = \left(\frac{\partial V}{\partial c} \right) \left(\frac{\partial c}{\partial n_2} \right)_{T, p, n_1} \rightarrow v = \frac{n_1 M_1 + n_2 M_2}{\rho} \quad \rho(c)_{T, p}$$

Vol. molar aparente

$$\bar{\Phi} = \frac{V - n_1 v_1^0}{n_2} = \bar{\Phi}(n_2)_{T, p, n_1}$$

$$L_2 v_2 = \bar{\Phi} + n_2 \left(\frac{\partial \bar{\Phi}}{\partial n_2} \right)_{T, p, n_1}$$

$$F^M = F'' - F' = T, p$$

$$h_i^M = \left(\frac{\partial H^M}{\partial n_i} \right)_{T, p, n_j} \quad H^M = Q \quad h_i^M = h_i - h_i^0$$

$$\mu_i = \left(\frac{\partial G}{\partial n_i} \right)_{T, p, n_j}$$

Mescl. ideales $\rightarrow \mu_1(T, p, x_2) = \mu_1^0(T, p) + RT \ln x_1$

No ideales $\rightarrow \mu_1(T, p, x_2) = \mu_1^0(T, p) + RT \ln \underbrace{\gamma_1}_{a_1} x_1$

$$\lim_{x_i \rightarrow 1} \gamma_i = 1$$

$$\mu_1 = \mu_1(T, p) + RT \ln \gamma_1 x_1$$

$$d \ln \gamma_1 = - \frac{n_2}{n_1} d \ln \gamma_2 \quad \mu_2 = \mu_2(T, p) + RT \ln \gamma_2 x_2$$

$$\lim_{x_1 \rightarrow 1} \gamma_2^a = 1$$

$$\lim_{x_2 \rightarrow 0} \gamma_2^a = 1$$

$$\gamma_2^a x_2^* = 1$$

$$\mu_2(T, p, x_2) = \mu_2(T, p, x_2^*) + RT \ln \gamma_2^a x_2$$

$$\mu_2(T, p, x_2) = \mu_2^{**}(T, p) + RT \ln \gamma_2^{(x)} x_2$$

$$\lim_{\frac{x_2}{m} \rightarrow 0} \gamma_2^{(x)} = 1$$

$$\mu_2(T, p, c) = \mu_2^{*c}(T, p) + RT \ln \gamma_2^{(c)} c$$

$$\frac{x_2}{m} \rightarrow 0$$

$$\mu_2(T, p, m) = \mu_2^{*m}(T, p) + RT \ln \gamma_2^{(m)} m$$

Diluidas

$$\mu_2^{**}(T, p) \rightarrow \mu_2^{*m}(T, p) = RT \ln \frac{1000}{M_1} \quad x_2 \approx \frac{m M_1}{1000}$$

$$\frac{\gamma_2^{(x)}}{\gamma_2^{(m)}} = \frac{M_1 m}{1000 x_2} = \frac{1}{1 - x_2}$$

$$G^M = G^U - G^I = RT \left(\sum n_i \ln \gamma_i x_i \right)$$

$$V = \left(\frac{\partial G}{\partial p} \right)_{T, n_i} \quad \frac{H}{T^2} = - \left(\frac{\partial G/T}{\partial T} \right)_{p, n_i}$$

$$V^M = RT \sum n_i \left(\frac{\partial \ln \gamma_i x_i}{\partial p} \right)_{T, n_i}$$

$$H^M = -RT^2 \sum n_i \left(\frac{\partial \ln \gamma_i x_i}{\partial T} \right)$$

$$X^E = X^M - X^{M_{id}} \dots \gamma_i = 1$$

$$m. \text{ ideal} \rightarrow V^{M_{id}} = 0, H^{M_{id}} = 0 \rightarrow V^E = V^M, H^E = H^M$$

$$G^E = RT \sum n_i \ln \gamma_i$$

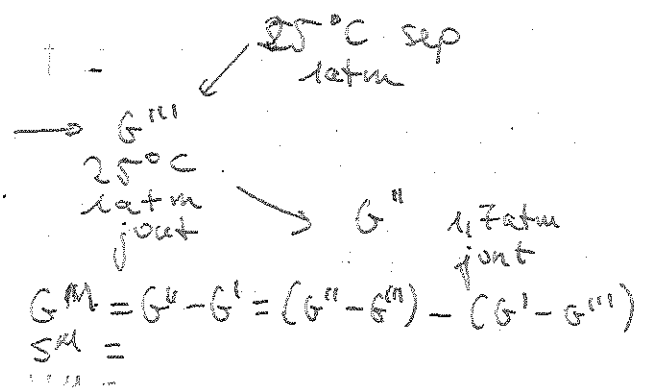
$$V^E = RT \sum n_i \left(\frac{\partial \ln \gamma_i}{\partial p} \right)_{T, n}$$

$$H^E = -RT^2 \sum n_i \left(\frac{\partial \ln \gamma_i}{\partial T} \right)_{p, n_i}$$

si T dan p konstan

$$\Delta G = -T \Delta S$$

$$S^M = -R \sum n_i \ln p_i x_i$$



TEMA 12

$$\Delta \mu_i = \mu_i^I - \mu_i^{II} \quad \begin{matrix} > 0 & I \rightarrow II \\ < 0 & II \rightarrow I \end{matrix}$$

$$= -\Delta \mu_i^0 + RT \ln \frac{a_i^I}{a_i^{II}}$$

$$\frac{d(\Delta \mu_i)}{dT} = \frac{\Delta h_{i0}}{T^2} dT - \frac{\Delta v_{i0}}{dT} dp + R d \ln \frac{a_i^I}{a_i^{II}}$$

$$\Delta \mu_i = 0 \rightarrow d \ln \frac{a_i^I}{a_i^{II}} = \frac{\Delta h_{i0}}{RT^2} dT - \frac{\Delta v_{i0}}{RT} dp$$

Líquidos $\rightarrow dp = 0, a_i^I = 1, a_i^{II} = a_i$

$$d \ln a_i = \frac{\Delta h_{i0}}{RT^2} dT$$

Diluida: $\Theta_c \approx \frac{R(T_1^0)^2 M_1}{1000 \Delta h_i} \cdot m = K_c \cdot m \quad K_2 \approx \frac{m M_1}{1000}$

L-V

$$d \ln \frac{x_i^V}{a_i} = \frac{\Delta h_{i0}}{RT^2} dT \quad \begin{matrix} \text{s. no volátil} \\ a_i \approx x_i \end{matrix} \rightarrow \Theta_c = \frac{RT_1^0 M_1}{1000 \Delta h_i} m$$

Δ L-V

$$a_i^{II} = x_i^V \rightarrow x_i^V p = a_i^I p_i^0 = p_i : \text{presión parcial}$$

\rightarrow Diluidas $p_1 = x_1 p_1^0$ Ley de Raoult (soluto)
 $y_2 = 1$
 $x_2^a = 1$ $p_2 = x_2 K_2$ " " Henry (disolvente)

\rightarrow No diluidas

$$p_2 = x_2 y_2^a K_2$$

Sim: $x_B^V p = y_B^S x_B^L p_B^0$

Asim: $x_B^V p = y_B^A x_B^L K$

Regla de las fases

$$W = 2 + K - \phi - r$$

Ley de Nernst $\rightarrow \frac{a_3^{II}}{a_3} = K \rightarrow$ diluidas $K = \frac{x_3^{II}}{x_3}$

Presión osmótica

$$\pi = p^{II} - p^I$$

diluida

$$\mu_1^0(p^I, T) = \mu_1^0(p^{II}, T) + RT \ln a_1$$

$$\mu_1(T, p, x_1) = \mu_1^0(T, p) + RT \phi \ln x_1 \quad \begin{matrix} \text{disolvente} \\ I \rightarrow II \end{matrix}$$

$$dn_i = \nu_i d\xi \rightarrow n_i - n_i^0 = \nu_i \xi$$

$$dG = \sum \nu_i \mu_i d\xi$$

$$A = -\sum \nu_i \mu_i \quad \left(\frac{dG}{d\xi}\right) = -A$$

Gas

$$\sum \nu_i \mu_i^* = -RT \sum \nu_i \ln \bar{p}_i = -RT \ln K$$

$$K = \prod p_i^{\nu_i} = \bar{p}^{\sum \nu_i} \prod x_i^{\nu_i} \quad 1, \dots, K$$

$$Q = \sum \nu_i h_i^0$$

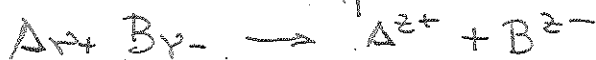
$$\frac{d \ln K}{dT} = \frac{Q}{RT^2} \rightarrow \text{Ecuación de Van't Hoff}$$

Disolución

$$\sum \nu_i \mu_i^* = -RT \ln a_i$$

$$K_a = \prod a_i^{\nu_i}$$

Sistemas electroquímicos



$$\nu_+ z_+ + \nu_- z_- = 0$$

$$n_2 \rightarrow n_+ = \nu_+ n_2$$

$$n_- = \nu_- n_2$$

$$\tilde{\mu}_i = \left(\frac{\partial G}{\partial n_i}\right)_{n_1, n_j} \quad i \neq j = +, -$$

$$\hookrightarrow \mu_i^0 = \mu_i^1$$

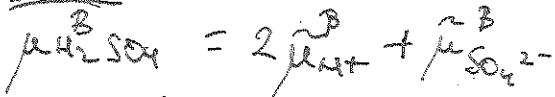
$$\tilde{\mu}_i^0 = \tilde{\mu}_i^1 \rightarrow \mu_2 = \nu_+ \tilde{\mu}_+ + \nu_- \tilde{\mu}_-$$

$$\nu = \nu_+ \nu_-$$

$$\mu_2 = \mu_2^* + \nu RT \ln a_2$$

↳ ions a partir electrolito

Pilas



$$\Delta\tilde{\mu}_e = \tilde{\mu}_e^w - \tilde{\mu}_e^x$$

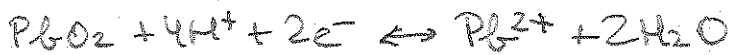
$$dW_{NE} = -F \Delta\psi \, dn_e$$

$$dG = (\mu_e^x - \mu_e^w) \, dn_e$$

$$\Delta\tilde{\mu}_e = -F \Delta\psi \quad \rightarrow \quad \Delta\psi = -\frac{\Delta\tilde{\mu}_e}{F}$$

Acumulador

$$\Delta\psi = \frac{\Delta}{nF} \quad n=2 \text{ plomo}$$



Pila de Daniell

$$\Delta\psi = \frac{\Delta - \Delta\tilde{\mu}_{SO_4^{2-}}}{2F}$$



$$\Delta\mu_{SO_4^{2-}}^{\delta-\delta}$$

Calor de reacción

$$Q = \sum \nu_i h_i^0$$

$$S = -\left(\frac{\partial \mu_i}{\partial T}\right)$$

$$\Delta = -\sum \nu_i \mu_i$$

$$\Delta = nF \Delta\psi$$

$$Q^* = \sum \nu_i h_i = nF \left[T \left(\frac{\partial \Delta\psi}{\partial T} \right)_{p, \dots} - \Delta\psi \right]$$

$$h_i^x = h_i - h_i^0$$

$$Q = Q^* - \sum \nu_i h_i^x \approx Q^*$$

$$\sigma = \frac{F}{e}$$

$$dW = p dV - \sigma d\Sigma$$

$$dU = T ds - p dV + \sigma d\Sigma$$

$$dF = -S dT + \sigma d\Sigma - \mu dn$$

Ley de Laplace:

$$p' - p'' = \frac{2\sigma}{r}$$



$$\sigma = \sigma^0 \left(1 - \frac{T}{T_c}\right)^\nu$$

T_{crit} des. interface
 $\nu = 1,27 \pm 0,02$

Buff-Lovett

$$p^L - p^V = \frac{2\sigma}{r}$$

$$\frac{V}{L} \quad r > 0$$

$$\frac{V}{L} \quad r < 0$$

$$\ln \frac{(p^V)_r}{(p^V)_\infty} = \frac{2\sigma v^L}{RTx}$$

TEMA 15

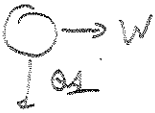
$$\Delta U = Q - W$$

$$\text{Ciclo} \rightarrow W = Q$$

Máquinas térmicas

2 focos

T_2
↓ Q_2



$$\eta = \frac{W}{Q_2} < 1$$

T_1

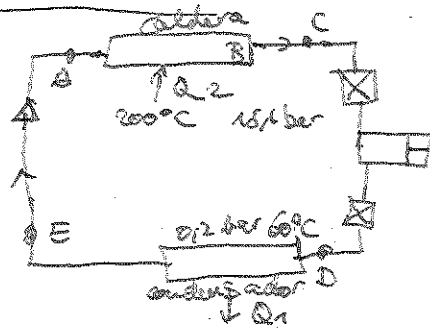
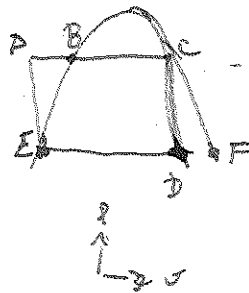
Máquina de vapor - Ciclo de Rankine

$$W = h_c - h_b$$

$$Q_2 = h_c - h_s$$

$$\eta = \frac{h_c - h_b}{h_c - h_s}$$

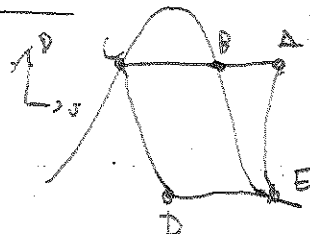
$$X_D = \frac{S_D - S_E}{S_F - S_E}$$



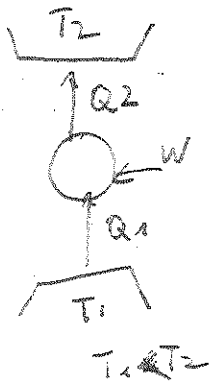
$$EA \rightarrow dh = v_e dp \rightarrow \Delta B \quad ds = \frac{C_p dT}{T} \Rightarrow \Delta T_A$$

Máquina frigorífica

$$\eta = \frac{Q_1}{W} \approx 1$$

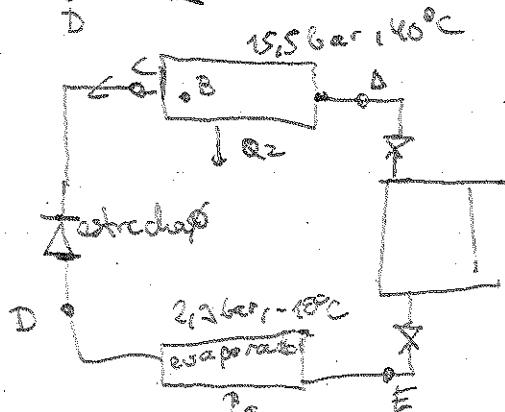


DC isob.
EA adiab.



Bomba calor

$$\eta = \frac{Q_2}{W} > 1$$



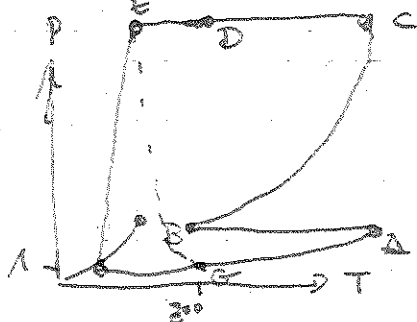
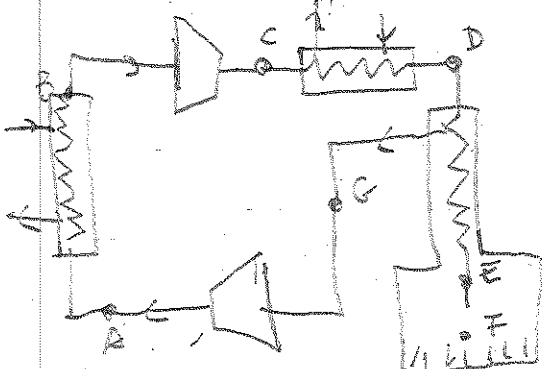
$$h_D = h_C$$

$$S_D = S_E$$

$$T_D = 115^\circ\text{C}$$

$$X_D = 0.18$$

Licuefacción de gases



$$\vec{j}_z \quad z = 1, 2, \dots, k, 0 = f(\vec{v}_T, \vec{v}_p, \vec{v}_{C2}, \vec{j}, \Delta \epsilon)$$

$$d^2 z = \vec{j}_z d\vec{\Delta} dt$$

$$\vec{j}_z = \lambda_{zT} \vec{v}_T + \lambda_{zP} \vec{v}_p + \lambda_{zC} \vec{v}_{C2} + \lambda_{zj} \vec{j}$$

$\Delta = 0$
 $\Delta \neq 0$

$j_z \rightarrow$ fl. termod.

$\vec{v} \rightarrow$ fuer "

$\lambda_{zi} \rightarrow$ coef. fuom. o dete.

Procesos termoeléctricos

$I, \frac{dT}{dx}$ Obs: $I, T, \Delta \psi$

Rel $\Rightarrow J_u, \frac{d\tilde{\mu}_e}{dx}$

$\Delta J_u = J_u^II - J_u^I$
 J_Q

S : coef. Seebeck = pot. termoeel.

Esteo $\rightarrow \Delta J_u = J_Q$

σ : conductividad eléctrica

$\Delta \psi = \psi^II - \psi^I$

π : coef. Peltier

$\tilde{\mu}_0 = \left(\frac{\partial G}{\partial N_e} \right)_{T, p, n_j}$

$N = n \cdot N_A$
 \downarrow
 $6.022 \cdot 10^{23}$

$J_u = K \Delta \frac{dT}{dx} + (\pi - \frac{\tilde{\mu}_e}{e}) I$

$\frac{d\tilde{\mu}_e}{e dx} = S \frac{dT}{dx} - \frac{\pi}{T \Delta}$

① L. Fourier $I=0, J_u = K \Delta \frac{dT}{dx}$

② Efecto Joule $I \neq 0, J_u = -\frac{\tilde{\mu}_e}{e} I = I \Delta \psi = W_{el} = J_Q$

③ Efecto Peltier $I \neq 0, \frac{dT}{dx} \neq 0$
 $J_Q \Rightarrow x < y > x \leftarrow I, J_u$
 $(J_u)_x = (J_u)_y$
 $\frac{(\pi_y - \pi_x) I}{A} = K_x \left(\frac{dT}{dx} \right)_x - K_y \left(\frac{dT}{dx} \right)_y$

④ Ley Ohm

$\frac{dT}{dx} = 0, I \neq 0 \rightarrow \Delta \psi = \frac{\Delta x}{\sigma A R} I$

⑤ Efecto Seebeck $\Delta \psi \neq 0, I=0, \frac{dT}{dx} \neq 0$

$\Delta \psi = \int_{T^I}^{T^{II}} (S_z - S_x) dT + R$



⑥ Coeficiente de Thomson $J_Q, I =cte$

$\Delta \left[K \Delta \frac{dT}{dx} \right] + I \int_{T^I}^{T^{II}} z dT + I \Delta \psi = J_Q$



$z(\Delta T) = \left(\frac{dT}{dT} - S \right)$

Formulación M.E.

Para $T\theta = \psi = J_s \frac{dT}{dx} + I \left(- \frac{d\tilde{\mu}_e/e}{dx} \right)$

\swarrow flujos \swarrow fuerzas

$\theta \equiv$ prod. entropía

Δ , trans. $\theta = 0$

inver. $\theta > 0$

$T J_s = J_u + I \left(\frac{\tilde{\mu}_e}{e} \right)$

$Q = \Delta U + W$

$\begin{pmatrix} J_s \\ I \end{pmatrix} = L \begin{pmatrix} dT/dx \\ -d\tilde{\mu}_e/e \end{pmatrix} \quad L_{12} = L_{21}$

RR0 $\Pi = TS \rightarrow \pi_x - \pi_y = T(S_x - S_y)$

$K = \frac{I}{A} \left(L_{11} - \frac{L_{12}L_{21}}{L_{22}} \right)$

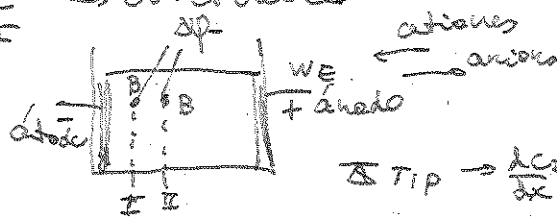
$\Pi = T \frac{L_{12}}{L_{22}} \quad \sigma = \frac{L_{21}}{L_{22}} \quad \rho = \frac{L_{22}}{A}$

Electrodifusión



1: dis, 2: sol. $\Delta r + B_1 \rightarrow \Delta^{z+}, B^{z-}$

$J_1, J_+, J_-, \Delta\psi = \frac{\Delta\mu_-}{z \cdot F} \rightarrow$ observables



$z \cdot \Delta\tilde{\mu}_e = -\Delta\tilde{\mu}_-$

$\Delta\psi = -\frac{\Delta\tilde{\mu}_e}{F} = \frac{\Delta\mu_-}{z \cdot F}$

$\Delta T_{IP} \rightarrow \frac{dc_2}{dx}, I \text{ o. ind}$



Ec. flu:

$\begin{pmatrix} J_1 \\ J_+ \\ J_- \end{pmatrix} = \begin{pmatrix} D_1 \Delta & \frac{z_1}{F} \\ D_2 \Delta & \frac{t_+}{v_+ z_+ F} \end{pmatrix} \begin{pmatrix} \frac{\Delta\psi}{dx} \\ \frac{dc_2}{dx} \end{pmatrix}$

D_i : \hookrightarrow difusión

z_1 : \hookrightarrow n.º transfer.

t_+ : \hookrightarrow n.º transp.

$I = 0 \rightarrow$ Dif. simple $\rightarrow \frac{J_+}{v_+} = \frac{J_-}{v_-} = J_2$

$\frac{dc_2}{dx} = 0 \rightarrow$ Proc. "cond. eléctrica" no definido J_2

Cond. eléctrica simple

$\frac{dc_2}{dx} = 0$

$J_+ = \frac{t_+}{z_+ F} I$

$t_+ = \frac{z_+ F J_+}{I}$

$t_+ t_- = 1$

$t_- = \frac{z_- F J_-}{I}$

$v_1 J_1 + v_2 \frac{J_+}{v_+} + \frac{v_0}{z_- F} I = 0$

$D_1 = -\frac{v_-}{v_+} D_2$

$z_1 = \frac{v_+ - v_0 - v_2 t_+}{v_+ z_1 v_1}$

$$\frac{J_+^1}{J_+} = \frac{J_+}{J_+} - \left(\frac{c_2}{c_1}\right) J_1$$

$$\begin{pmatrix} J_+^1 \\ I \end{pmatrix} = L \begin{pmatrix} d\mu_2/dx \\ d\psi/dx \end{pmatrix}$$

$$L_{12} = L_{21}$$

$$\frac{L_{11}}{L_{22}} = \frac{t_+}{z_+ z_+ F}$$

$$t_+^1 = -\frac{z_+ F}{z_+ F} \left(\frac{d\psi}{dx} \right)_{I=0}$$

$$\frac{d\psi}{dx} = \alpha - \frac{dc_2}{dx} + \frac{I}{\sigma}$$

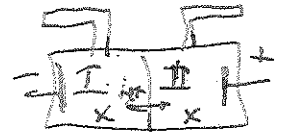
$$\alpha = \frac{t_+^1}{z_+ z_+ F} \frac{d\mu_2}{dc_2}$$

Electrodifusión en membranas.

T, pcte

$$\Delta c_2, I, \frac{dc_2}{dx}$$

$$t_+ + t_- = 1$$



$$J_1 = p_1 \Delta c_2 + \frac{z_1 I}{F}$$

$$\Delta \psi = \frac{\Delta \mu_-}{z_- F} = \delta \Delta c_2 + R_1$$

$$\frac{J_+}{J_+} = p_2 \Delta c_2 + \frac{t_+}{z_+ z_+ F} I$$

$$\Delta \tilde{\mu}_- = z_- F \Delta \psi$$

$$\Delta \tilde{\mu}_+ = \frac{\Delta \mu_+}{z_+} + z_+ F \Delta \psi$$

$$\psi = J_1 \Delta \mu_1 + \frac{J_+}{J_+} \Delta \mu_2 + I \Delta \psi = \frac{J_+^1}{J_+} \Delta \mu_2 + I \Delta \psi$$

$$\frac{J_+^1}{J_+} = \frac{z_+}{z_+} - \frac{c_2}{c_1} J_1$$

$$\begin{pmatrix} \frac{J_+^1}{J_+} \\ I \end{pmatrix} = P \begin{pmatrix} \Delta \mu_2 \\ \Delta \psi \end{pmatrix}$$

$$P_{12} = P_{21} \quad \frac{P_{12}}{P_{22}} = \frac{t_+^1 F}{z_+ z_+ F}$$

$$t_+^1 = -\frac{z_+ F \Delta \psi}{\Delta \mu_2}$$

Electrodialisis

membrana $\left\{ \begin{array}{l} K \\ \Delta \end{array} \right. \quad \begin{array}{l} t_+^K \approx 1 \\ t_-^\Delta \approx 1 \end{array}$

$$J_1 = J_1^K - J_1^\Delta$$

$$J_2 = (J_+^K - J_+^\Delta) / z_+$$

$$\Delta c_2 = c_2^K - c_2^\Delta$$

$$p_1 = p_1^K + p_1^\Delta$$

$$p_2 = p_2^K + p_2^\Delta$$

$$\Delta z_1 = z_1^K - z_1^\Delta$$

$$\Delta t_+ = t_+^K - t_+^\Delta$$

$$J_1 = p_1 \Delta c_2 + \frac{\Delta z_1 I}{F}$$

$$J_2 = p_2 \Delta c_2 + \frac{\Delta t_+}{z_+ z_+ F} I$$



$$1 \text{ atm} = 1,01325 \times 10^5 \text{ Pa}$$

$$1 \text{ mmHg} = 133,322 \text{ Pa}$$

$$1 \text{ bar} = 10^5 \text{ Pa}$$

$$1 \text{ psi} = 6,89476 \times 10^3 \text{ Pa}$$

$$1 \text{ cal} = 4,1868 \text{ J}$$

$$R = 8,31441 \text{ J/molK}$$

$$= 1,9862 \text{ cal/molK}$$

$$= 0,08209 \frac{\text{atm dm}^3}{\text{molK}}$$

$$N_A = 6,023 \cdot 10^{23} / \text{mol}$$

$$dU = n c_v dT + \left[T \left(\frac{\partial p}{\partial T} \right)_v - p \right] dV$$

$$dH = n c_p dT + \left[v - T \left(\frac{\partial v}{\partial T} \right)_p \right] dp$$

$$dS = \frac{n c_v dT}{T} + \left(\frac{\partial p}{\partial T} \right)_v dV$$

$$= \frac{n c_p dT}{T} - \left(\frac{\partial v}{\partial T} \right)_p dp = \frac{n c_p}{T} \left(\frac{\partial T}{\partial v} \right)_p dV + \frac{n c_v}{T} \left(\frac{\partial T}{\partial p} \right)_v dp$$

$$dU = n c_v dT + \left[T \frac{\alpha}{\kappa} - p \right] dV$$

$$dH = n c_p dT + v(1 - \alpha T) dp$$

$$dS = \frac{n c_v dT}{T} + \frac{\alpha}{\kappa} dV$$

$$dS = \frac{n c_p}{T} dT - \alpha v dp = \frac{n}{\alpha T} \left[C_p \frac{dV}{v} + \kappa \alpha v dp \right]$$

$$C_p - C_v = \frac{T v \alpha^2}{\kappa}$$

$$dU = T ds - p dV + \mu du$$

$$dF = -S dT - p dV + \mu du$$

$$dH = +T ds + v dp + \mu du$$

$$dG = -S dT + v dp + \mu du$$

$$U = TS - pV + \mu u$$

$$F = U - TS = -pV + \mu u$$

$$G = \mu u = F + pV$$

$$d\mu = -s dt + v dp$$

pára y uotas
 páto y uotep
 vapo páto
 vota páto v

$\kappa = \chi$